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- (E) Catalyst and process for dehydrating 2-alcohols.
- There is also disclosed a novel process for obtaining high purity 4-methyl-1-pentene involving the dehydration of 4-methyl-2-pentanol followed by disproportionation with ethylene.

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CATALYST AND PROCESS FOR DEHYDRATING 2-ALCOHOLS

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Background of the Invention

This invention relates to the production of α -olefins by the catalytic dehydration of 2-alcohols.

It is well known that a'cohols may be dehydrated to produce monooletinic materials by passing the alcohols over the heated oxides of certain metals, such as aluminum oxide, thorium oxide, silicon dioxide, titanium oxide, magnesium oxide, tungsten oxide, chromium oxide, and zirconium oxide or mixtures thereof. The prior technical literature on the subject of this type of catalytic dehydration indicates that alumina, thoria and several of the other metal oxides are equivalents in their dehydrating effect and usually may be used interchangeably. Pines and Haag have reported in a paper published at page 2847 of volume 83 of the Journal of the American Chemical Society (1961) that α -olefins (terminally unsaturated olefins) may be obtained by dehydrating primary alcohols over an alumina catalyst. These workers further state that when 2-alcohols are dehydrated over the alumina catalyst, a mixture of internal olefin and α olefin results, with the more stable internal olefin predominating over the a-olefin. Obtaining a dehydration product in which the a-olefin predominates significantly is a challenge since the internal olefin product is the thermodynamically favored product.

U.S. 3,283,027 discloses that thorium oxide and a number of other metal oxides including cerium oxide and other oxides of the rare earths possess the capability of catalyzing the selective dehydration of 2-alcohols to α -olefins.

Such catalysts have been found to have several disadvantages. For example, thorium oxide is a very insoluble material which makes it a difficult material to apply to a support. Further, when thorium oxide was applied to glass bead support as shown in Example 4 of that patent, it was noted that the catalyst was quite fragile and that thoria fell off the glass beads and caused reactor plugging. When the thorium oxide-glass bead catalyst was employed as a catalyst in the dehydration of 4methyl-2-pentanol, it was noted that at atmospheric pressure the conversion was quite low even at high reaction temperature. In order to actually be commercially attractive, the dehydration catalyst should be durable and should give good conversion and selectivity at atmospheric pressure.

An object of the present invention is to provide a dehydration catalyst that is durable and that is capable of giving good conversion and selectivity to α -olefin even at atmospheric pressure.

Another object is to provide a method for the production of 4-methyl-1-pentene and 3-methyl-1-butene in various ratios from 4-methyl-2-pentanol and ethylene.

Summary of the Invention

in accordance with the present invention, there is provided a catalyst for the selective dehydration of 2-alcohols to α-olefins comprising a catalytically effective amount of at least one metal oxide wherein the metal is selected from the group consisting of metals having atomic numbers of 21, 39, 58-71, or 90 supported on a support comprising an oxide of alumina and further being characterized by having a surface area no greater than 20 m²/gm as determined by the BET nitrogen adsorption technique.

In accordance with yet another embodiment of the present invention, there is provided a catalyst for the selective dehydration of 2-alcohols to α -olefins comprising a catalytically effective amount of a mixture of thorium oxide and cerium oxide supported on a support comprising a base treated oxide of alumina.

In accordance with yet another embodiment of the present invention, there is provided a method for the production of 4-methyl-1-pentene and 3-methyl-1-butene by the dehydration of 4-methyl-2-pentanol over a dehydration catalyst and then contacting the resulting mixture of 4-methyl-1-pentene and 4-methyl-2-pentene with ethylene in the presence of a disproportionation catalyst under conditions sufficient to promote conversion of 4-methyl-2-pentene to a mixture of 3-methyl-1-butene and propylene, wherein said dehydration catalyst is selective to 4-methyl-1-pentene production when large yields of 4-methyl-1-pentene are desired or to 4-methyl-2-pentene when large yields of 3-methyl-1-butene are desired.

Detailed Description

The support used in the preferred embodiment of the present invention can be any suitable support containing an oxide of alumina which has a surface area no greater than about 20 m²/gm, preferably no greater than 5 m²/gm. Included within the scope of the invention are thus the low surface area aluminas and combinations of aluminum oxide and silicon oxide having low surface area. The preferred supports are those comprising α-alumina, especially those having a surface area of no great-

er than 1 m²/gm. in a particularly preferred embodiment, the support is treated with a basic compound of a metal of Groups I and II of the Periodic Table.

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The catalytically active metal oxides that are deposited on the defined support are selected from the group consisting of thorium oxide, scandium oxide, yttrium oxide, and the oxides of the rare earth metals, cerium, praseodymium, neodymium, prometheum, samarium, europium, gadolinium, terbium, dysprosium, holmium, erbium, thulium, ytterbium, and lutecium. Typical examples include Ce₂O₃, CeO₂, Dy₂O₃, Er₂O₃, Eu₂O₃, EuO, Gd₂O₃, Ho_2O_1 , Lu_2O_3 , Nd_2O_3 , Pr_2O_3 , PrO_2 , Pr_6O_{11} , Sm_2O_3 , SmO, Tb_2O_3 , TbO_2 , Tb_4O , Tm_2O_3 , Yb_2O_3 , YbO. Se₂O₃, Y₂O₃, and ThO₂.

The catalyst is considered to be effective for the dehydration of any 2-alcohol that is capable of being dehydrated to an alpha olefin. Examples of such 2-alcohols are those of the formula

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wherein at least one R is hydrocarbon in nature and wherein each R is individually selected from the group consisting of hydrogen, hydrocarbon radicals, and substituted hydrocarbon radicals wherein the substituents are selected from the keto, hydroxyl, alkoxy, and ester groups. Typically in order for 2-alcohols to be capable of being dehydrated to alpha olefins, aryl groups should be attached only at the number 4 position or a higher position, keto groups should be attached only at the number 5 position or a higher position, carboncarbon elefinic or acetylenic unsaturation, hydroxyl groups, and ester groups should be attached only at the number 6 or higher position and preferably the number 7 or higher position. Obviously, the R on the 2 position carbon must be either H or a methyl group in order for the alcohol to be a 2alcohol.

Typically, the hydrocarbyl radicals and the substituted hydrocarbyl radicals in the above formula would contain 1 to 17 carbon atoms. Generally, the preferred 2-alcohols are those in which the R of the number 2 position is hydrogen or a methyl group and at least one of the other R's is hydrogen and the remaining R group is selected from alkyl, cycloalkyl, or aralkyl groups having 1 to 17 carbon atoms, more preferably 1 to 10 carbon atoms.

The upper limit on the total carbon number of the suitable 2-alcohols is basically related to their ability to be vaporized under reasonable conditions. Thus extremely high boiling alcohols would be difficult if not impossible to use. Under very high vacuum, it is conceivable that alcohols having 30, 40, and even 50 carbon atoms per molecule could be employed. However, the preferred alcohols are those having no more than 20 carbon atoms per molecule.

A list of typical 2-alcohols meeting the requirements of the preceding general formula are disclosed in columns 3 and 4 of U.S. 3,283,027, the disclosure of which is incorporated herein by reference.

The catalytic metal oxides can be deposited on the support in any suitable manner known in the art. The most common technique involves the deposition of a salt of the catalytic metal on the support followed by decomposition of the salt to an oxide of the catalytic metal. The currently preferred technique involves the use of a nitrate of the catalytic metal. An aqueous solution of the metal nitrate is poured over the support. After soaking for 30 minutes to an hour, the solution is concentrated by evaporation, and then the support containing the catalytic metal is dried in the presence of oxygen under such conditions that the metal salt is converted to the metal oxide. Typically, this involves heating in air at a temperature in the range of 300°C to about 600°C.

The amount of catalytic metal oxide that can be employed in the present invention can vary over a wide range, with any catalytically effective amount being suitable. Typically, the total amount of the above defined catalytically active metal oxide is such that the total amount of the metal of catalytic metal oxide is in the range of about 0.5 to about 30 weight percent based on the weight of the support. More preferably, the total amount of the metal of the catalytic metal oxide is in the range of about 2 to about 25 weight percent based on the weight of the support.

A particularly preferred embodiment of the present invention involves the employment of a catalyst containing both cerium and thorium. In such catalysts, it is generally preferred for the weight percent of thorium to be in excess of the weight percent of the cerium. Typically for best

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results, the weight ratio of thorium to cerium should be in the range of 1/2 to 30/1, more preferably about 1/1 to 10/1. In such catalysts particularly good results have been obtained using about 5 to about 20 weight percent thorium based on the weight of the support.

As mentioned earlier, a particularly preferred embodiment of this invention involves the use of a support that has been treated with a basic compound of a metal of Groups I and II of the Periodic Table. The amount of basic compound that can be employed can vary over a wide range; however, the conversion in the dehydration reaction appears to be inversely related to the level of basic compound. Accordingly, it is generally preferred that the amount of basic compound deposited on the support be no more than about 4 weight percent based on the weight of the support prior to the base treatment. Typical examples of basic compounds of Groups I and II include potassium hydroxide, cesium carbonate, sodium hydroxide, calcium hydroxide, and magnesium carbonate. The presently preferred basic compound is potassium hydroxide.

Since many of the preferred catalysts of the present invention employ a support that has been base treated, it is here noted that in this disclosure and the foregoing claims when a reference is made to the amount of a particular metal component, such as thorium, in terms of weight percent based on the weight of the support that is intended to refer to the weight of the support prior to any base treatment.

The basic compound can also be added to the support in any suitable manner. Presently, the preferred technique involves soaking the support with an aqueous solution of the basic compound prior to the addition of the catalytic metal.

Another embodiment of the present invention is based upon the discovery that one can obtain a catalyst having high selectivity to α-olefin even with aluminum oxide-containing supports having surface areas greater than 20 m²/gm by subjecting the support to base treatment and depositing thorium oxide and cerium oxide thereon. The techniques of catalyst preparation and the levels of the various catalyst components are the same as set forth previously for the catalysts prepared from the low surface area supports. Examples of such larger surface area supports are those alumina supports consisting essentially of alumina and having sur-

face area in the range of about 100 to about 350 $\,\mathrm{m}^2/\mathrm{gm}$.

In the dehydration of 2-alcohols with the catalysts of the present invention, the alcohol in a vapor state is passed in contact with the catalyst. The temperature at which the reaction is conducted is determined by a number of variables, the most important of which are the nature of the alcohol reactant, the residence time, and the extent of conversion desired. These variables can be readily ascertained for each alcohol by those skilled in the art by routine tests.

Generally, however, reaction temperature in the range of 330°C to 600°C are suitable, with temperatures in the range of 350°C to 450°C being preferred. The present catalysts can be employed at subatmospheric pressures and superatmospheric pressures, but are most desirable since even at atmospheric pressure they allow conversions and selectivities that were not attainable with the prior art catalysts.

A further understanding of the present invention and its advantages will be provided by the following examples. In the following examples, unless stated otherwise, if the aluminum oxide support is base treated, the general technique employed involved soaking 100 gm of the support with a 50 mL aqueous solution of a basic compound such as KOH for about 30 minutes. The liquid was poured off and the support washed three times with 50 to 100 mL aliquots of water.

The catalytically active metal was added to the support, after the base treatment, if a base treated support was employed. The general technique involved soaking 100 gms of the support with 50 mL of an aqueous solution of a nitrate of the catalytically active metal. After soaking for about 30 minutes, the solution was concentrated by evaporation, and then the support was dried in air at about 350°C for about 3 hours.

The dehydration reactions were carried out in a reactor tube ½" in diameter and 20" long that was packed with 40 gm of the catalyst. Alcohol reactant was introduced into the reactor tube at a rate of 36 mL/hr. A nitrogen sweep of 60 mL/min was employed.

Several different aluminum oxide containing supports are used in the following examples. The following table sets forth some of the characteristics of the supports:

		U	omposition	Suriace Area,	
Support	Manufacturer	<u>A1203</u>	SiO ₂	<u>Na</u> 20	m ² /gm
R268*	Norton	86.0	12.4	-	0.6
T1370	Girdler	95.0	.1-1.0	.3-3.0	188.0
H151	Alcoa	98.0	1.2	0.7	324.0
60-503	Union Carbide (Linde)	99.85	0.1	0.003	215
61-501	Union Carbide (Linde)	99.75	0.15	0.01	230

*A Phillips' identification number for Norton's SA-5123.

Example I

In one experiment, 0.6 weight percent Li was deposited on the Linde 60-503 support in the form of an aqueous solution of lithium hydroxide. After soaking for about 30 minutes, the solution was concentrated by evaporation and the support dried in air at 120°C for about 8 hours. The resulting base-treated support was then evaluated as a catalyst for the dehydration of 4-methyl-2-pentanol at atmospheric pressure. At temperatures of 300°C and 310°C, the conversion of the alcohol was 100%. About 99.5 percent of the alcohol was converted to olefins. However, the 4-methyl-1-pentene,

accounted for no more than 39.2 percent of the olefins whereas the internal olefin isomer, 4-methyl-2-pentene accounted for 60 to 62 percent of the olefin product. This illustrates that the base-treated alumina oxide alone is selective for the more thermodynamically favored internal olefin.

Example II

In another experiment, a series of catalysts were prepared by treating various aluminum oxide supports with thorium nitrate. The catalysts were then employed in the dehydration of 4-methyl-2-pentanol. The results are summarized in Table I.

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Table I

Support Th, Wt.%** Temp,°C Press_rest Alcohol Conversion,% Olefin Selectivity,*% R268 19.3 400 Atm. 89.6 82.4 95.8 3.9 R268 19.3 410 Atm. 98.4 89.3 94.3 4.0 T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
Support Th, Wt.%** Temp,°C Press_e Conversion,% 18tar 425 R268 19.3 400 Atm. 89.6 82.4 95.8 3.9 R268 19.3 410 Atm. 98.4 89.3 94.3 4.0 T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
Support In, wt.km Lary R268 19.3 400 Atm. 89.6 82.4 95.8 3.9 R268 19.3 410 Atm. 98.4 89.3 94.3 4.0 T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0 T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
R268 19.3 400 Atm. 98.4 89.3 94.3 4.0 R268 19.3 410 Atm. 98.4 89.3 94.3 4.0 T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
R268 19.3 410 Atm. 98.4 556 T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
T1370 9.7 290 30 psig 15.6 n.d. n.d. n.d. T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
T1370 9.7 290 30 psig 13.0 T1370 9.7 330 30 psig 57.7 n.d. n.d. n.d. T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
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T1370 9.7 365 30 psig 92.4 90.2 59.3 40.0
T13/0 9.7 a.d. n.d.
20.0 30 psig 8 H.u. 200
T13/0 19.5 20 n.d. n.d. n.d.
T1370 19.3 330 36 P525 82.4 46.2 53.5
m1370 19 3 350 30 psig 92.1
100 99 31.3 6/.2
1151*** 5.3 280 ncm.
300 Atm. 99.5
HISTAN 98.6 96.6 27.8 00.9
H151*** 5.3 320 Atm. College tables. Total is the percent of alcohol

*In this table and the following tables, <u>Total</u> is the percent of alcohol converted to olefin. The values under 4-MP-1 and 4-MP-2 refer to the percentage of the total olefin product represented by that particular olefin.

**Weight percent of Th as metal, based on the weight of the support.
***Thorium solution also contained 6 weight percent oxalic acid.

This example indicates that the effect of thorium on the dehydration reaction is much different for the low surface area support than the higher surface area supports. The ratio of the 4-methyl-1-pentene to the 4-methyl-2-pentene is surprisingly higher for the low surface area support, i.e., Norton's R268.

Example III

Another experiment was conducted using a series of catalysts prepared by treating those supports with potassium hydroxide and then with thorium nitrate. The effects of those catalysts on the dehydration of 4-methyl-2-pentanol are set fort in Table II.

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Table II

				Alcohol		Select	ivity,%
Th, Wt.%	K, Wt.%	Temp, °C	Pressure	Conversion,%	Tctal	4-MP-1	4-MP-2
19.3	2.8	370	Atm.	37.0	36.1	99.3	0.4
19.3	2.8	402	Atm.	69.7	67.1	99.2	0.4
19.3	2.8	412	Atm.	75.2	71.6	99.5	0.3
19.3	2.8	422	Atm.	85.5	81.3	99.6	0.3
19.3	2.8	434	Atm.	93.0	87.9	99.6	0.3
19.3	2.8	444	Atm.	95.6	90.2	99.4	0.3
19.3	2.8	446	Atm.	90.9	85.8	99.4	0.4
19.3	1.4	340	30 psig	13.0	n.d.	n.d.	n.d.
19.3	1.4	370	30 psig	29.8	28.8	99.0	0.5
19.3	1.4	397	30 psig	51.5	48.8	99.2	0.4
	19.3 19.3 19.3 19.3 19.3 19.3 19.3	19.3 2.8 19.3 2.8 19.3 2.8 19.3 2.8 19.3 2.8 19.3 2.8 19.3 1.4 19.3 1.4 19.3 1.4	19.3 2.8 370 19.3 2.8 402 19.3 2.8 412 19.3 2.8 422 19.3 2.8 434 19.3 2.8 444 19.3 2.8 446 19.3 1.4 340 19.3 1.4 370	19.3 2.8 370 Atm. 19.3 2.8 402 Atm. 19.3 2.8 412 Atm. 19.3 2.8 422 Atm. 19.3 2.8 434 Atm. 19.3 2.8 444 Atm. 19.3 2.8 446 Atm. 19.3 1.4 340 30 psig 19.3 1.4 370 30 psig	Th, Wt.% K, Wt.% Temp, °C Pressure Conversion,% 19.3 2.8 370 Atm. 37.0 19.3 2.8 402 Atm. 69.7 19.3 2.8 412 Atm. 75.2 19.3 2.8 422 Atm. 85.5 19.3 2.8 434 Atm. 93.0 19.3 2.8 444 Atm. 95.6 19.3 2.8 446 Atm. 90.9 19.3 1.4 340 30 psig 13.0 19.3 1.4 370 30 psig 29.8	Th, Wt.% K, Wt.% Temp, °C Pressure Conversion,% Tctal 19.3 2.8 370 Atm. 37.0 36.1 19.3 2.8 402 Atm. 69.7 67.1 19.3 2.8 412 Atm. 75.2 71.6 19.3 2.8 422 Atm. 85.5 81.3 19.3 2.8 434 Atm. 93.0 87.9 19.3 2.8 444 Atm. 95.6 90.2 19.3 2.8 446 Atm. 90.9 85.8 19.3 1.4 340 30 psig 13.0 n.d. 19.3 1.4 370 30 psig 29.8 28.8	Th, Wt.% K, Wt.% Temp, °C Pressure Conversion,% Total 4-MP-1 19.3 2.8 370 Atm. 37.0 36.1 99.3 19.3 2.8 402 Atm. 69.7 67.1 99.2 19.3 2.8 412 Atm. 75.2 71.6 99.5 19.3 2.8 422 Atm. 85.5 81.3 99.6 19.3 2.8 434 Atm. 93.0 87.9 99.6 19.3 2.8 444 Atm. 95.6 90.2 99.4 19.3 1.4 340 30 psig 13.0 n.d. n.d. 19.3 1.4 340 30 psig 29.8 28.8 99.0

A comparison of the results in Table II with those in Table I reveals that the base treatment of the supports results in a slight decrease in the overall conversion of the alcohol but an increase in the selectivity to the alpha olefin. Accordingly, by using the base treatement and slightly higher reaction temperatures, one can obtain higher yields of the alpha olefin than can be obtained at similar levels of alcohol conversion with a catalyst of thorium on a support which had not been base treated.

20 Example IV

Another catalyst was prepared by depositing thorium and cerium on the Norton R268 support. The thorium was deposited in an amount equal to 19.3 weight percent of the support. The cerium was deposited in an amount equal to 3.2 weight percent of the support. The effectiveness of this catalyst in the dehydration of 4-methyl-2-pentanol at atmospheric pressure is shown in Table III.

Table III

	Alcohol	0lefi	n Selectiv	ity, %
Temp, °C	Conversion, %	Total	4-MP-1	4-MP-2
370	65.1	61.8	98.8	neg.
400	92.1	86	98.7	neg.
410	96.7	91	98.9	neg.

A comparison of the results of Table III with those in Tables I and II reveals that the alcohol conversion is slightly better for the Th-Ce catalyst than for the corresponding Th-base treated catalyst of Table II and the selectivity to 4-methyl-1-pentene is slightly better for the Th-Ce catalyst than for the corresponding non-base treated Th catalyst of Table I.

45 Example V

In yet another series of runs, 19.3 weight percent thorium and 3.2 weight percent cerium were deposited on aluminum oxide supports that were pretreated with KOH. The results obtained when the catalysts were used to dehydrate 4-methyl-2pentanol at atmospheric pressure are shown in Table IV.

Table IV

	Tr 1.14 9/	Temp, °C	Alcohol Conversion, %	Olefin Total	Selectiv 4-MP-1	<u>ity, %</u> <u>4-MP-2</u>
Support	K, Wt.% 2.8	370	63.6	61.8	99.3	neg.
R268 R268	2.8	400	89.2	86.2	99.6	neg.
R268	2.8	410	95.4	91.6	99.6	neg.
R268	1.4	370	64.9	62.6	99.6	neg.
R268	1.4	390	84.9	80.8	99.6	neg.
R268	1.4	410	96.7	91.1	99.6	neg.
60-501	1.4	400	73.7	69.4	99.6	0.4
60-501	1.4	420	90.2	84	84.6	14.7

A comparison of the results obtained with the low surface area Norton R268 support in this example with the results of Example IV, reveals that while the alcohol conversion is slightly lower for the base treated Th-Ce catalyst of this Example than for the Th-Ce catalyst of Example IV, the selectivity to the alpha olefin is slightly better. Accordingly, where high yields of the α-olefin are desired, the preferred catalyst would be one having been treated with Th, Ce, and base.

The above results also show that the combination of Th, Ce, and base can even improve the 4-MP-1 selectivity of a catalyst prepared from the higher surface area Linde 61-501 support. In Example II, it will be recalled, the high surface area Th-containing supports gave olefin products in which

the α -olefin was either less than half of the olefin product or only slightly more than half.

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Example VI

Another series of catalysts were employed in the dehydration of 2-methyl-2-butanol. All the reactions were carried out at atmospheric pressure, employing a 36 mL/hr feed rate of 2-methyl-2-butanol, and 60 mL/min nitrogen flow rate. Reaction temperature, feed alcohol conversions and selectivities to 2-methyl-1-butene are set fortin in Table V. The major reaction by-product is 2-methyl-2-butene.

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Table V

Cupport	Th, Wt.%	Ce, Wt.%	K, Wt.%	Temp, °C	Alcohol Conversion, %	α-Olefin,% [*]
Support	19.3		0.7	350	99	64.3
R268		_	0.3	350	99.1	57.9
R268	19.3	. –	7.0	350	6.8	n.d.
R268	10.0	-		450	81.6	85.4
R268	10.0	•	- ^		85.8	95.4
R268	19.3	3.2	2.8	360		97.5
R268	19.3	3.2	2.8	380	99.5	37.3
60-503	_	_	0.7	310	98.0	47.5
	_	-	7.0	310	82.1	56.5
60-503	_					

*Percentage of olefin product.

The above data reveals that the selectivity to α -olefin of the base treated low surface area Th-containing catalyst was better than that of the base

treated high surface area catalyst. The data further illustrates that the selectivity to the α -olefin is even better if Ce is employed in conjunction with the Th

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and base treatment.

Example VII

The data presented in the foregoing examples and the prior art make it quite clear that in the dehydration of 4-methyl-2-pentanol, it is possible to obtain wide variations in the ratio of alpha olefin to internal olefin by the use of various types of catalysts. This fact can be applied to provide a process for the coproduction of selected ratios of 4-methyl-1-pentene and 3-methyl-1-butene, two specialty chemicals for which there is considerable demand. The process involves the dehydration of the 4methyl-2-pentanol to obtain a mixture of 4-methyl-1-pentene and 4-methyl-2-pentene followed by the disproportionation of that olefin mixture with ethylene. Typically, it is desirable to remove substantially all the other dehydration reaction products and unreacted alcohol from the mixture of 4methyl-1-pentene and 4-methyl-2-pentene prior to subjecting that mixture to the disproportionation reaction. Any suitable conditions can be employed in the disproportionation reaction. Typical conditions are disclosed in U. S. Patents 3,457,320 and 3,658,932, the disclosures of which are incorporated herein by reference.

Thus, if one employs a dehydration catalyst of the type disclosed herein which gives an olefin product in which substantially all the olefin is 4methyl-1-pentene, the coproduction process results mainly in 4-methyl-1-pentene. The coproduction process does however allow for the recovery of a more pure 4-methyl-1-pentene since it is much easier to separate 3-methyl-1-butene from 4-methyl-1-pentene by distillation than it is to separate 4-methyl-2-pentene from 4-methyl-1-pentene.

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By employing a dehydration catalyst that gives an approximately 1:1 ratio of 4-MP-1 to 4-MP-2, one can obtain a product from the metathesis reaction, a product having 4-MP-1, 3-MB-1, and propylene in about a 1:1:1 ratio.

By employing a dehydration catalyst that gives about a 2:1 ratio of 4-MP-2 to 4-MP-1, one can obtain a product from the metathesis reaction having a 3-MB-1 to 4-MP-1 ratio of around 2/1.

Accordingly by simply varying the dehydration catalyst, it is possible to vary the relative yields of 3-MB-1 and 4-MP-1 over a wide range. A corresponding benefit is that the 4-MP-1 can be more readily recovered as a substantially pure product than it can from the reaction product of the dehydration reaction.

Example VIII

Another series of catalysts were prepared using Th and Ce and other base treated low surface area aluminum oxide containing supports obtained from Norton. The supports and their relevant properties are summarized in Table VI.

Table VI Composition, Wt. % Surface Area, SiO2 m₂/gm Support 0.3 SA-5102 87 11 0.7 99 SA-5158 80 18 14 SA-3235

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These catalysts, like the other previously discussed inventive catalysts, gave conversions of more than 90% with the 4-MP-1 product being the predominant olefin formed. The selectivity to 4-MP-1 was lower for the higher surface area support SA-3235.

The following part of the description are preferred embodiments 1 to 27 presented in the format of claims.

- A catalyst for the dehydration of alcohols comprising a base treated support comprising aluminum oxide having deposited thereon a catalytically effective amount of a mixture of thorium oxide and cerium oxide.
- 2. A catalyst according to claim 1 wherein said support has a surface area in the range of 100 to $350 \, \text{m}^2/\text{gm}$.
- A catalyst according to claim 2 containing about 5 to about 20 weight percent of thorium metal based on the weight of the support and

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further being characterized by containing cerium in such an amount that the weight ratio of thorium to cerium is in the range of 1/2 to 30/1.

- 4. A catalyst according to claim 3 containing about 19 weight percent thorium metal based on the weight of said support and about 3 weight percent cerium metal based on the weight of said support.
- 5. A catalyst according to claim 4 wherein said support has a surface area of about 230 m²/gm and comprises about 99.75 weight percent alumina.
- 6. A catalyst according to claim 5 wherein the base treatment was provided by potassium hydroxide and the level of potassium is about 1.4 weight percent based on the weight of the support.
- 7. A catalyst for the dehydration of alcohols comprising a catalytically effective amount of at least one catalytic metal oxide of metals selected from the group consisting of metals having atomic numbers of 21, 39, 58-71, or 90 supported on a support comprising an oxide of alumina, said support further being characterized by having a surface area no greater than 20 m²/gm.
- 8. A catalyst according to claim 7 wherein the total amount of said catalytic metal oxide is in the range of 0.5 to about 30 weight percent based on the weight of the support.
- 9. A catalyst according to claim 8 containing thorium oxide.

- 10. A catalyst according to claim 9 wherein the catalytic metal oxide consists essentially of thorium oxide.
- A catalyst according to claim 9 containing thorium oxide and cerium oxide.
- 12. A catalyst according to claim 11 wherein the catalytic metal oxide consists essentially of thorium oxide and cerium oxide, the level of thorium is in the range of about 5 to about 20 weight percent based on the weight of the support, and the weight ratio of thorium to cerium is in the range of about 1/2 to about 30/1.
- 13. A catalyst according to claim 12 wherein the support has been base treated.
- 14. A catalyst according to claim 13 wherein potassium hydroxide is used in the base treatment.
- 15. A catalyst according to claim 8 wherein the support has been base treated.
- 16. A catalyst according to claim 15 wherein potassium hydroxide is used in the base treatment.
- 17. A catalyst according to claim 16 containing thorium oxide.
- 18. A process for preparing α -olefins comprising contacting a 2-alcohol that is capable of being dehydrated to a α -olefin under suitable reaction conditions with a catalyst as set forth in claims 1-17.
- 19. A process according to claim 18 wherein said 2-alcohol has less than 30 carbon atoms per molecule.
- 20. A process according to claim 19 wherein said 2-alcohol is of the formula

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wherein the R in the 2 position is hydrogen or a methyl radical and the other R is an alkyl, cycloal-kyl, or aralkyl group having 1 to 17 carbon atoms.

- 21. A process according to claim 20 wherein said 2-alcohol consists essentially of 4-methyl-2-pentanol.
- 22. A process according to claim 20 wherein said 2-alcohol consists essentially of 2-methyl-2-butanol.
- 23. A process for the production of 4-methyl-1-pentene comprising dehydration of 4-methyl-2-pentanol over a dehydration catalyst and then contacting the resulting mixture of 4-methyl-1-pentene and 4-methyl-2-pentene with ethylene in the presence of a disproportionation catalyst under con-

ditions sufficient to convert said 4-methyl-2-pentene to a mixture of 3-methyl-1-butene and propylene.

- 24. A process according to claim 23 wherein the 4-methyl-1-pentene in the reaction product of the disproportionation reaction is separated from the remainder of the reaction product.
- 25. A process according to claim 24 wherein the dehydration catalyst is one which results in a reaction product in which the ratio of 4-methyl-1-pentene to 4-methyl-2-pentene is about 1/1.
- 26. A process according to claim 24 wherein the dehydration catalyst is one which results in a reaction product in which the ratio of 4-methyl-1-pentene to 4-methyl-2-pentene is about 1/2.

27. A process according to claim 24 wherein said dehydration catalyst is a catalyst as set forth in claims 1-17.

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Claims

- A catalyst for the dehydration of alcohols comprising at least one catalytic metal oxide of metals having atomic numbers of 21, 39, 58-71, or 90, supported on a support comprising alumina, characterized by said support having a surface area no greater than 20 m²/gm.
- 2. The catalyst of claim 1 characterized in that the total amount of said catalytic metal oxide is in the range of 0.5 to 30 weight percent based on the weight of the support.
- The catalyst of claim 1 or 2 characterized by containing thorium oxide, or thorium oxide and cerium oxide.
- 4. The catalyst of any of the preceding claims characterized in that the catalytic metal oxide consists essentially of thorium oxide and cerium oxide, the level of thorium is in the range of 5 to 20 weight percent based on the weight of the support, and the weight ratio of thorium to cerium is in the range of 1:2 to 30:1; in particular wherein the

support has been base treated; in particular wherein potassium hydroxide is used in the base treatment.

- 5. The catalyst of any of the preceding claims characterized by containing about 19 weight percent thorium metal based on the weight of said support and about 3 weight percent cerium metal based on the weight of said support.
- 6. The catalyst of any of the preceding claims characterized in that said catalyst is prepared by soaking a support comprising alumina having a surface area no greater than 20 m³/g with an aqueous solution of potassium hydroxide, then washing the support with water, then washing the support with an aqueous solution of cerium nitrate and thorium nitrate, then evaporating the water, and then calcining at a temperature in the range of 300 to 600°C.
- 7. A process for preparing α -olefins comprising contacting a 2-alcohol capable of being dehydrated to an α -olefin under dehydration conditions with a catalyst, characterized by using a catalyst of one of claims 1 to 6.
- 8. The process of claim 7, characterized in that said 2-alcohol has less than 30 carbon atoms per molecule; in particular wherein said 2-alcohol is of the formula

wherein the R in the 2 position is hydrogen or a methyl radical and the other R is an alkyl, cycloal-kyl, or aralkyl group having 1 to 17 carbon atoms.

- 9. The process of claim 8 characterized in that said 2-alcohol consists essentially of 4-methyl-2-pentanol or wherein said 2-alcohol consists essentially of 2-methyl-2-butanol.
- 10. The process of claim 8 characterized in that after dehydration of 4-methyl-2-pentanol the resulting mixture of 4-methyl-1-pentene and 4-

methyl-2-pentene is contacted with ethylene in the presence of a disproportionation catalyst to convert said 4-methyl-2-pentene to a mixture of 3-methyl-1-butene and propylene; in particular wherein the 4-methyl-1-pentene in the reaction product of the disproportionation reaction is separated from the remainder of the reaction product.

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EUROPEAN SEARCH REPORT

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